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(54)	SYSTEM FOR MANAGEMENT OF YEAST TO
	FACILITATE THE PRODUCTION OF
	ETHANOL

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(57) ABSTRACT

A system and method for managing an ethanologen for use in biorefinery is disclosed. The method for propagating ethanologen for use in the production of a fermentation product from biomass comprises the steps of providing a medium for propagation of ethanologen and supplying a first cell mass of ethanologen to the medium. A first cell mass of ethanologen is propagated into a larger second cell mass of ethanologen.

21 Claims, 20 Drawing Sheets

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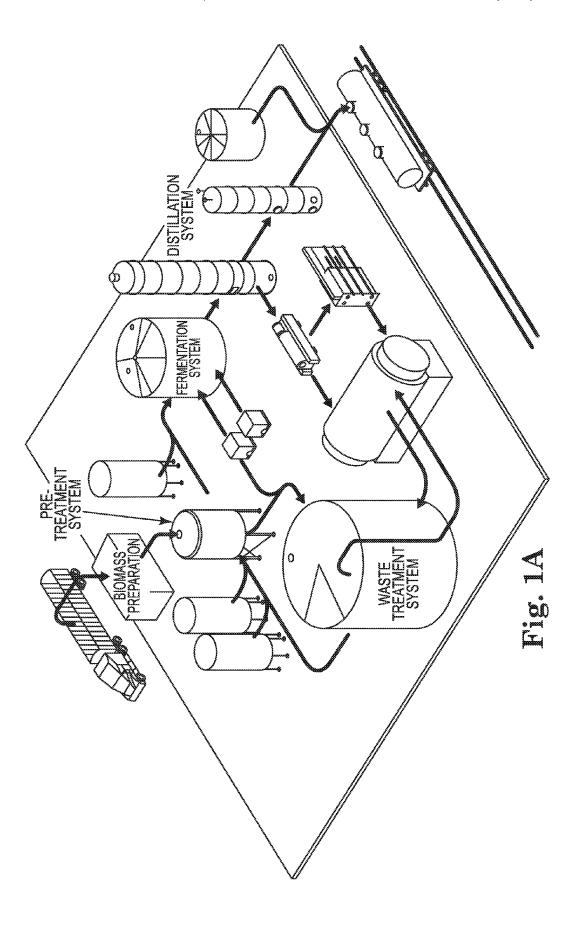
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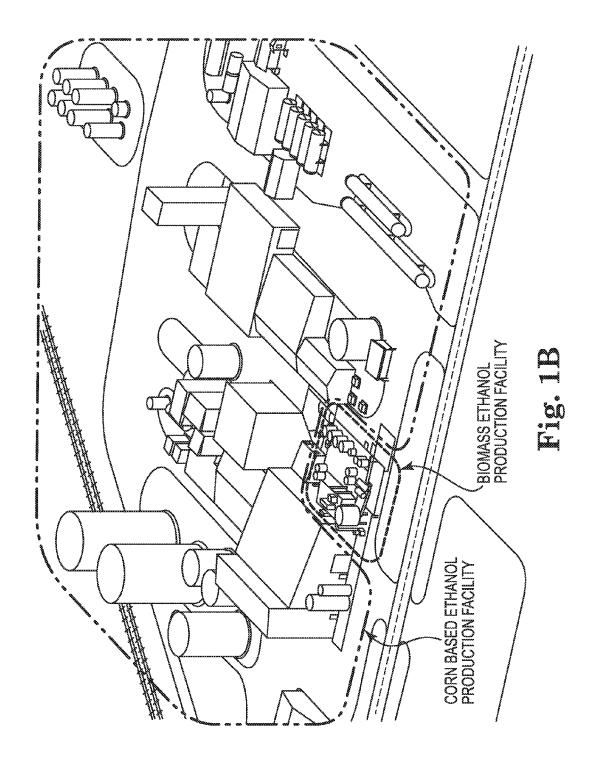
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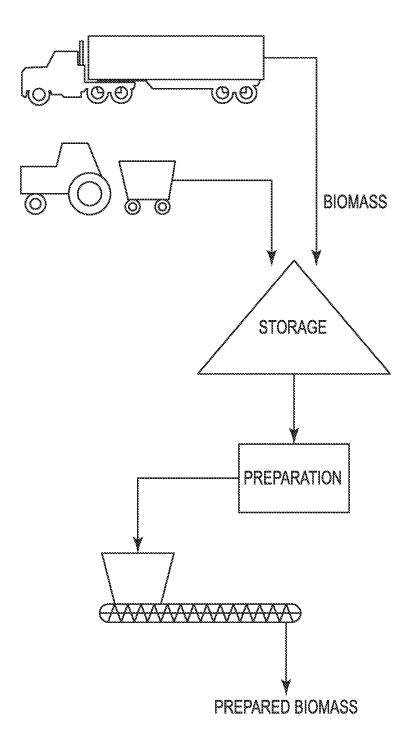


Fig. 2

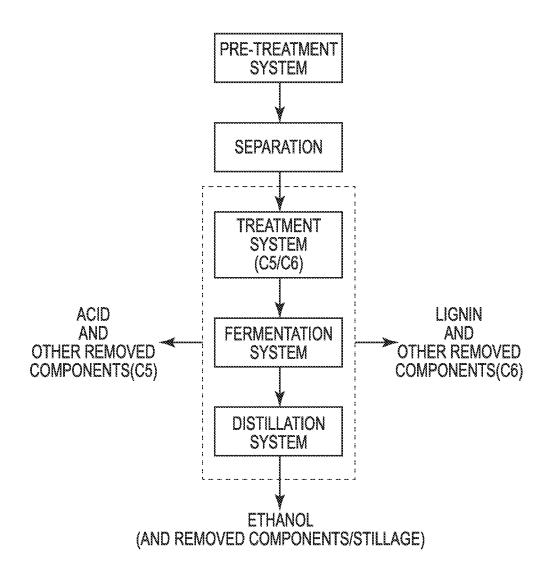
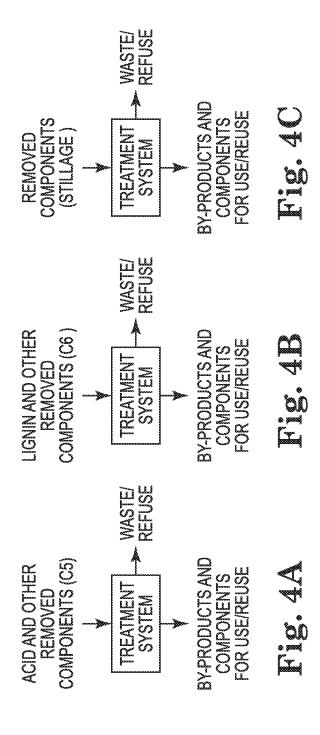


Fig. 3



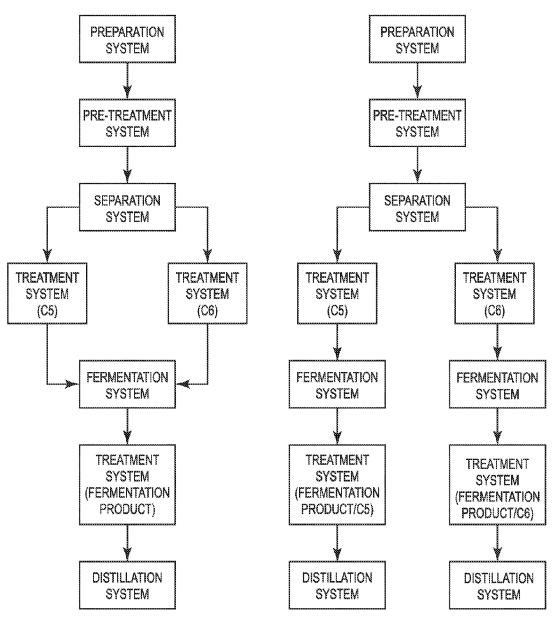


Fig. 5A Fig. 5B

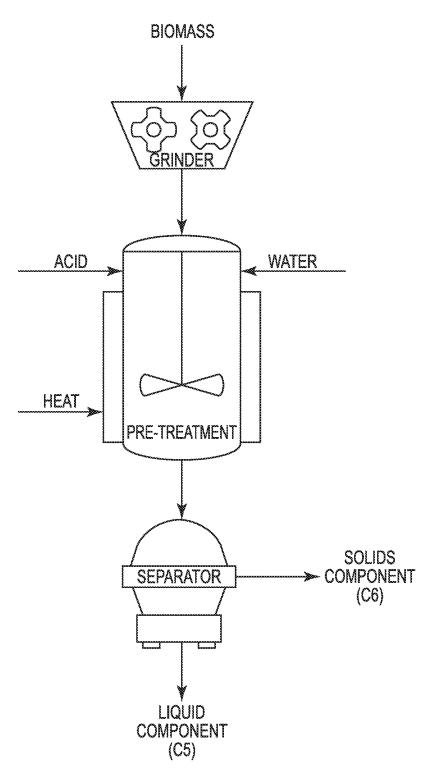
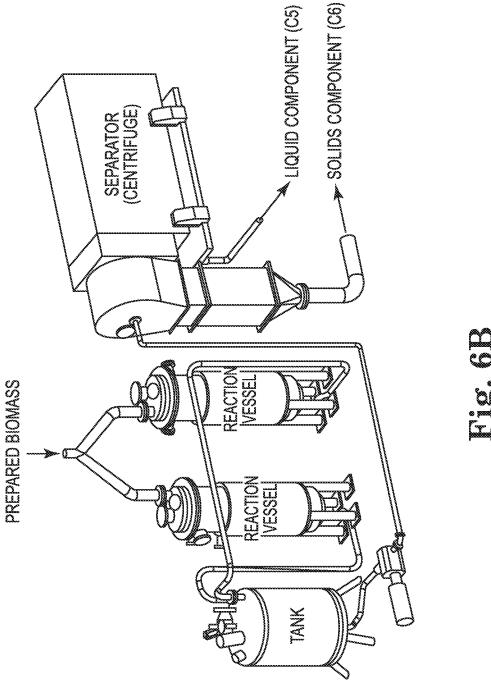


Fig. 6A



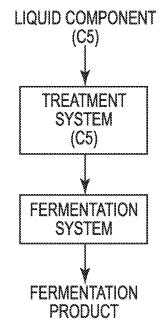


Fig. 7A

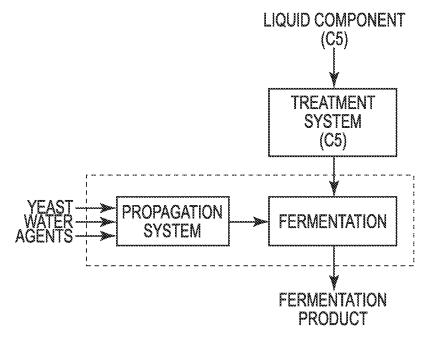
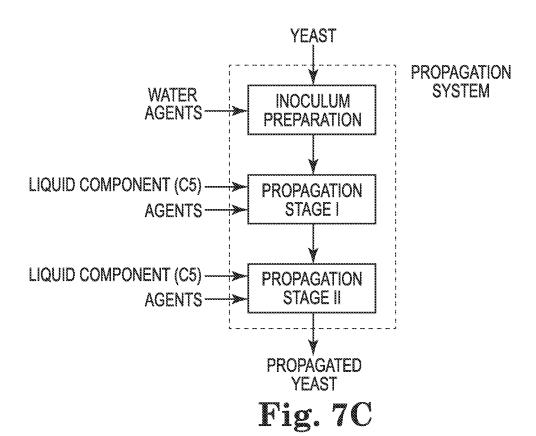
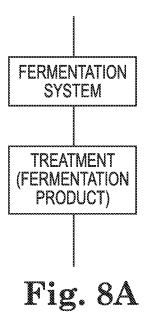


Fig. 7B





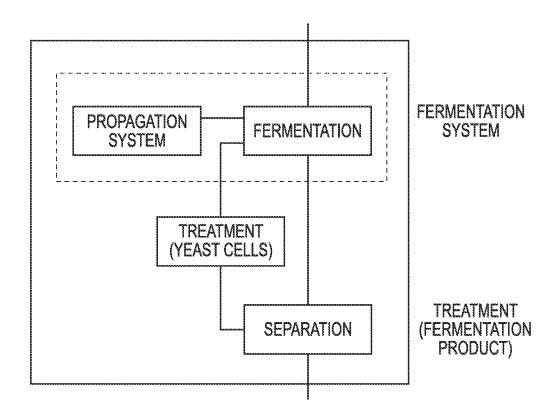


Fig. 8B

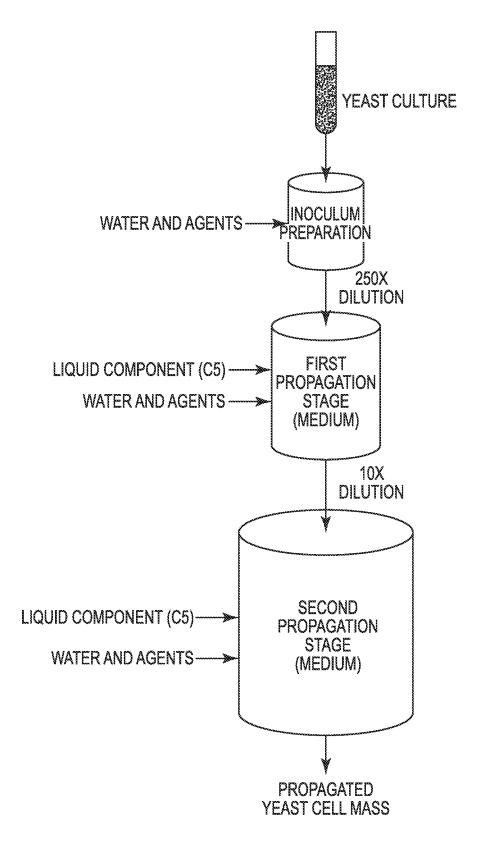


Fig. 9

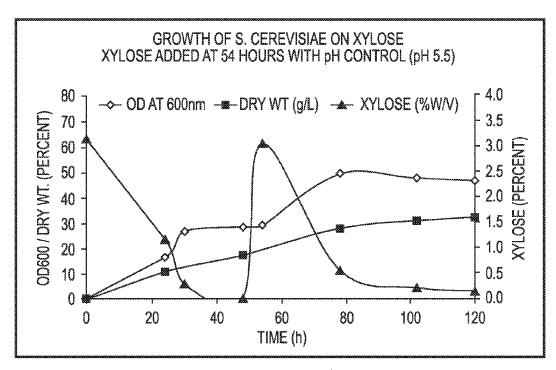


Fig. 10A

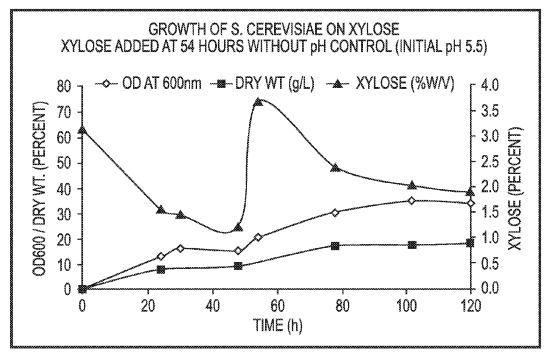


Fig. 10B

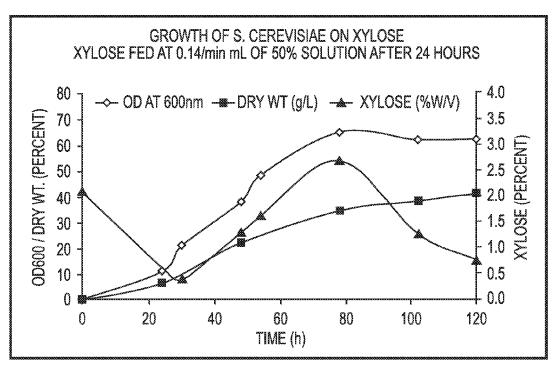


Fig. 11A

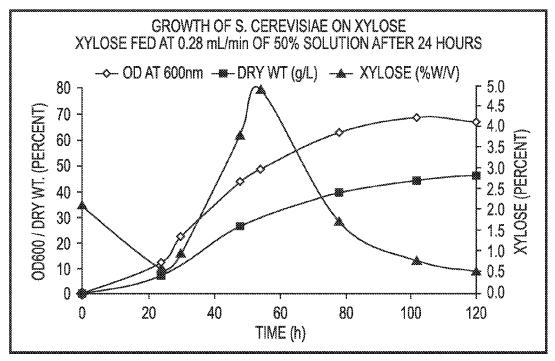


Fig. 11B

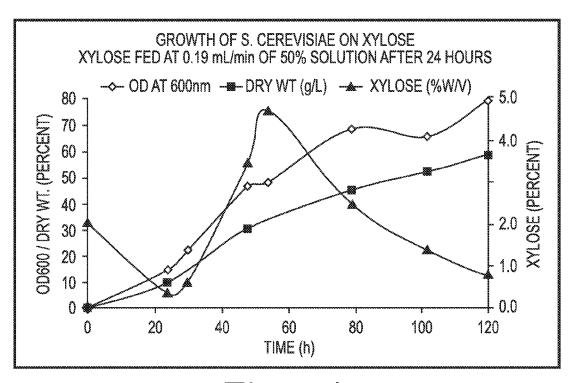


Fig. 12A

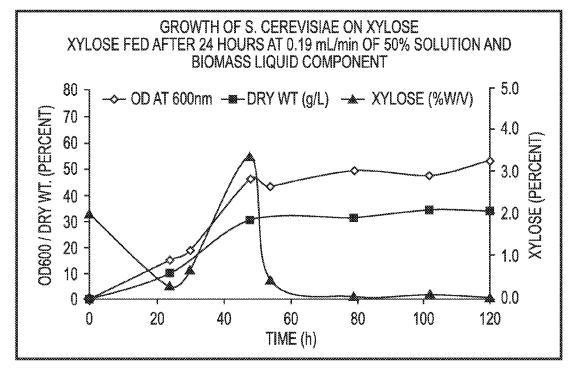


Fig. 12B

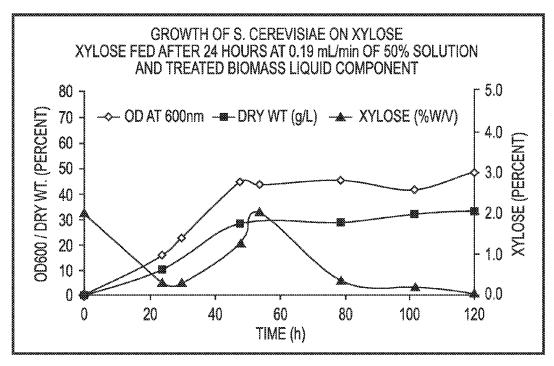


Fig. 12C

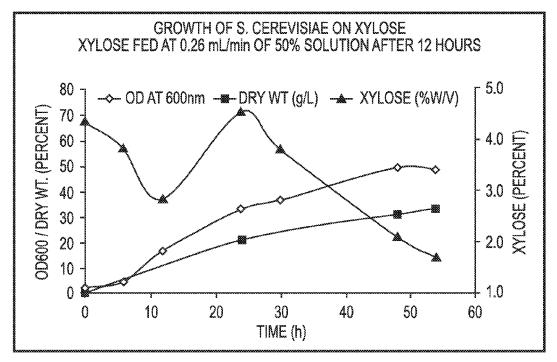


Fig. 13A

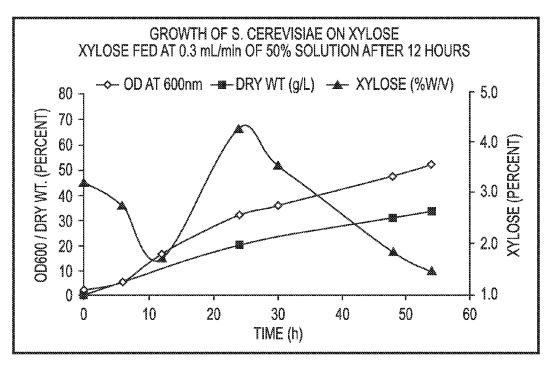


Fig. 13B

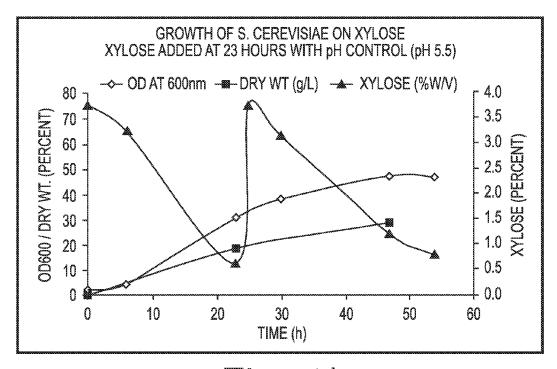


Fig. 14A

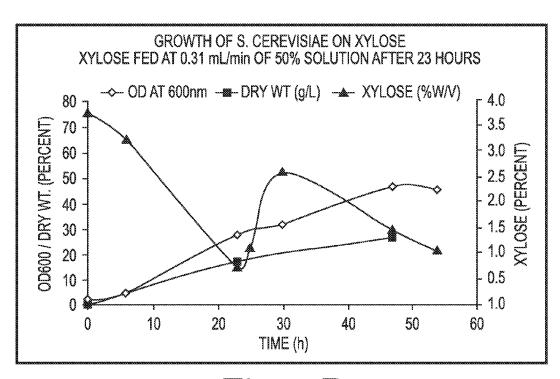


Fig. 14B

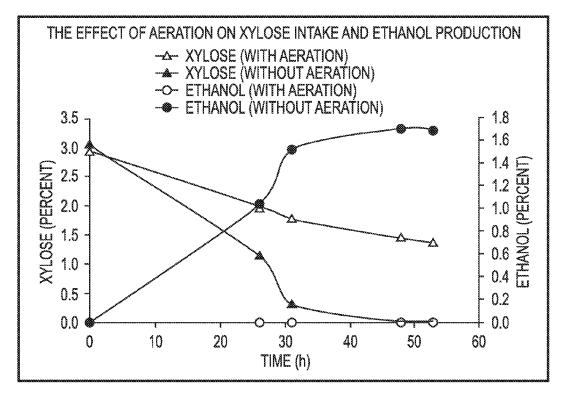


Fig. 15A

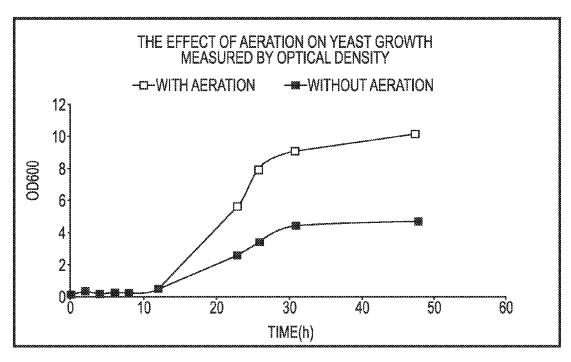


Fig. 15B

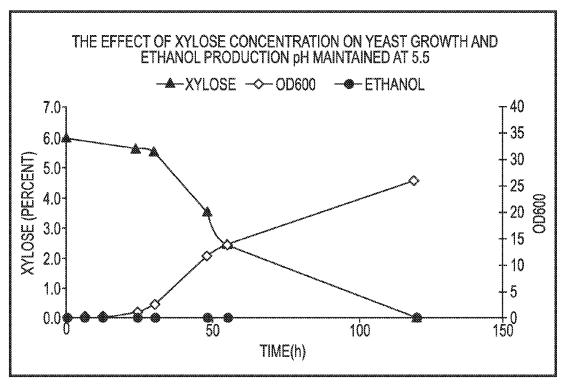


Fig. 16A

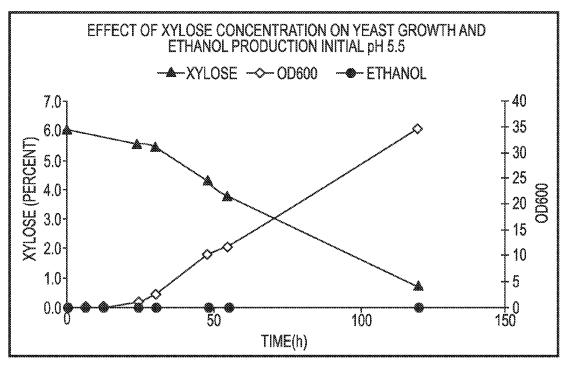


Fig. 16B

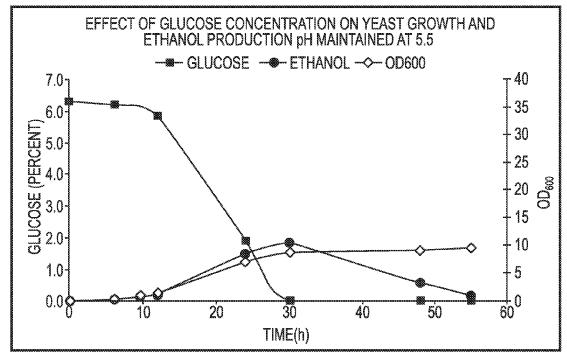


Fig. 16C

SYSTEM FOR MANAGEMENT OF YEAST TO FACILITATE THE PRODUCTION OF ETHANOL

CROSS-REFERENCE TO RELATED APPLICATIONS

The present application claims priority to and incorporates by reference each of the following applications: U.S. Provisional Application Ser. No. 61/157,151, titled Propagation of ¹⁰ Pentose Metabolizing Yeast Cells, filed on Mar. 3, 2009.

The present application is related to and incorporates by reference the following published applications: (a) U.S. Publication No. US 2010/0233771, titled System for Pre-Treatment of Biomass for the Production of Ethanol, filed on Mar. ¹⁵ 3, 2010; and (b) U.S. Publication No. US 2010/0227369, titled System for Fermentation of Biomass for the Production of Ethanol, filed on Mar. 3, 2010.

FIELD

The present invention relates to a system for the production of cellulosic ethanol and recovery of other bioproducts. The present invention also relates to a system for management of yeast to facilitate the production of ethanol. The present 25 invention further relates to a method of propagating ethanologen for use in the production of a fermentation product from biomass.

BACKGROUND

Ethanol can be produced from grain-based feedstocks (e.g. corn, sorghum/milo, barley, wheat, soybeans, etc.), from sugar (e.g. from sugar cane, sugar beets, etc.), and from biomass (e.g. from lignocellulosic feedstocks such as switch- 35 grass, corn cobs and stover, wood or other plant material).

Biomass comprises plant matter that can be suitable for direct use as a fuel/energy source or as a feedstock for processing into another bioproduct (e.g., a biofuel such as cellulosic ethanol) produced at a biorefinery (such as an ethanol 40 plant). Biomass may comprise, for example, corn cobs and stover (e.g., stalks and leaves) made available during or after harvesting of the corn kernels, fiber from the corn kernel, switchgrass, farm or agricultural residue, wood chips or other wood waste, and other plant matter (grown for processing into 45 bioproducts or for other purposes). In order to be used or processed, biomass will be harvested and collected from the field and transported to the location where it is to be used or processed.

In a conventional ethanol plant producing ethanol from 50 corn, ethanol is produced from starch. Corn kernels are cleaned and milled to prepare starch-containing material for processing. (Corn kernels can also be fractionated to separate the starch-containing material (e.g. endosperm) from other matter (such as fiber and germ).) The starch-containing mate- 55 rial is slurried with water and liquefied to facilitate saccharification where the starch is converted into sugar (e.g. glucose) and fermentation where the sugar is converted by an ethanologen (e.g. yeast) into ethanol. The product of fermentation (i.e. fermentation product) is beer, which comprises a liquid 60 component containing ethanol and water and soluble components, and a solids component containing unfermented particulate matter (among other things). The fermentation product is sent to a distillation system. In the distillation system, the fermentation product is distilled and dehydrated into etha- 65 nol. The residual matter (e.g. whole stillage) comprises water, soluble components, oil and unfermented solids (i.e. the sol2

ids component of the beer with substantially all ethanol removed that can be dried into dried distillers grains (DDG) and sold as an animal feed product). Other co-products, for example syrup (and oil contained in the syrup), can also be recovered from the stillage. Water removed from the fermentation product in distillation can be treated for re-use at the plant.

In a biorefinery configured to produce ethanol from biomass, ethanol is produced from lignocellulosic material. Lignocellulosic biomass typically comprises cellulose, hemicellulose and lignin. Cellulose (a type of glucan) is a polysaccharide comprising hexose (C6) sugar monomers such as glucose linked in linear chains. Hemicellulose is a branched chain polysaccharide that may comprise several different pentose (C5) sugar monomers (such as xylose and arabinose) and small amounts of hexose (C6) sugar monomers in branched chains.

The biomass is prepared so that sugars in the lignocellulosic material (such as glucose from the cellulose and xylose from the hemicellulose) can be made accessible and fermented into a fermentation product from which ethanol can be recovered. After fermentation the fermentation product is sent to the distillation system, where the ethanol is recovered by distillation and dehydration. Other bioproducts such as lignin and organic acids may also be recovered as by-products or co-products during the processing of biomass into ethanol. Determination of how to more efficiently prepare and treat the biomass for production into ethanol will depend upon the source and type or composition of the biomass. Biomass of 30 different types or from different sources is likely to vary in properties and composition (e.g. relative amounts of cellulose, hemicellulose, lignin and other components). For example the composition of wood chips will differ from the composition of corn cobs or switchgrass.

It would be advantageous to provide for a system for the production of cellulosic ethanol. It would also be advantageous to provide a system for management of yeast to facilitate the production of ethanol. It would further be advantageous to provide for a system that provides one or more features to facilitate improvement in the efficiency and yield of cellulosic ethanol from biomass.

SUMMARY

The present invention relates to a method of propagating ethanologen for use in the production of a fermentation product from biomass. The method comprises the steps of providing a medium for propagation of ethanologen; supplying a first cell mass of ethanologen to the medium; supplying xylose to the medium as a carbon source for the ethanologen; and maintaining the medium comprising the first cell mass of ethanologen at a pH of between about 5.0 and 6.0 and at a temperature of between about 26 and about 37 degrees Celsius so that the first cell mass of ethanologen is propagated into a second cell mass of ethanologen. The second cell mass of ethanologen is larger than the first cell mass of ethanologen.

The present invention also relates to a method of propagating ethanologen for use in the production of a fermentation product from biomass. The method comprises the steps of providing a medium for propagation of ethanologen; supplying a first cell mass of ethanologen to the medium; providing an agent to the medium; providing a component obtained from the biomass to the medium as a carbon source for the ethanologen; and maintaining the medium comprising the first cell mass of ethanologen at a pH of between about 5.0 and 6.0 and at a temperature of between about 26 and about. 37

degrees Celsius so that the first cell mass of ethanologen is propagated into a second cell mass of ethanologen. The second cell mass of ethanologen is larger than the cell mass of the first amount of ethanologen. The biomass comprises lignocellulosic material; the lignocellulosic material comprises at least one of corn cobs, corn plant husks, corn plant leaves and corn plant stalks. The component is obtained from the lignocellulosic material; the component comprises pentose. Pentose comprises the carbon source for the ethanologen. The ethanologen comprises yeast cells capable of fermenting pentose into ethanol.

The present invention further relates to a system for propagating ethanologen for use in the production of a fermentation product from biomass in a fermentation system. The system comprises a first stage comprising a first vessel configured to $\,^{15}$ maintain a medium comprising ethanologen; a second stage comprising a second vessel configured to maintain a medium supplied from the first stage; a source of xylose to be provided to the medium as a carbon source for ethanologen in the first stage; and a source of xylose to be provided to the medium as 20 a carbon source for the ethanologen in the second stage. The ethanologen has a first cell mass when supplied to the first stage and the ethanologen has a second cell mass when supplied from the first stage to the second stage and the ethanologen has a third cell mass when supplied from the second stage. 25 The medium in the first vessel is maintained at a pH of between about 5.0 and 6.0 and at a temperature of between about 26 and about 37 degrees Celsius so that ethanologen can be propagated into the second cell mass; the medium in the second vessel is maintained at a pH of between about 5.0 30 and 6.0 and at a temperature of between about 26 and about 37 degrees Celsius so that ethanologen can be propagated into the third cell mass. The second cell mass is at least 200 times larger than the first cell mass. The third cell mass is at least 20 times larger than the second cell mass.

BRIEF DESCRIPTION OF THE FIGURES AND TABLES

FIG. 1A is a perspective view of a biorefinery comprising 40 a cellulosic ethanol production facility.

FIG. 1B is a perspective view of a biorefinery comprising a cellulosic ethanol production facility and a corn-based ethanol production facility.

FIG. 2 is a schematic diagram of a system for receipt and 45 preparation of biomass for a cellulosic ethanol production facility.

FIG. 3 is a schematic block diagram of a system for the production of ethanol from biomass.

FIGS. 4A, 4B and 4C are schematic block diagrams of 50 systems for treatment and processing of components from the production of ethanol from biomass.

FIGS. 5A and 5B are schematic diagrams of the process flow for systems for the production of ethanol from biomass.

FIG. 6A is a schematic block diagram of apparatus used for 55 preparation, pre-treatment and separation of biomass.

FIG. 6B is a perspective view of apparatus used to pre-treat and separate the biomass.

FIG. 7A is a schematic block diagram of the process flow for a system for the production of a fermentation product from 60 a liquid component (C5).

FIG. 7B is a schematic block diagram of the process flow of a system according to an exemplary embodiment.

FIG. 7C is a schematic block diagram of the process flow of a system according to an exemplary embodiment.

FIG. 8A is a schematic block diagram of the process flow of a system according to an exemplary embodiment.

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FIG. 8B is a schematic block diagram of the process flow of a system according to an exemplary embodiment.

FIG. 9 is schematic diagram of a system according to an exemplary embodiment.

FIG. 10A is a line graph showing the growth of ethanologen using xylose.

FIG. 10B is a line graph showing the growth of ethanologen using xylose.

FIG. 11A is a line graph showing the growth of ethanologen.

FIG. 11B is a line graph showing the growth of ethanologen.

FIG. 12A is a line graph showing the growth of ethanologen using xylose.

FIG. 12B is a line graph showing the growth of ethanologen using xylose and a biomass liquid component.

FIG. 12C is a line graph showing the growth of ethanologen using xylose and a treated biomass liquid component.

FIG. 13A is a line graph showing the growth of ethanologen using xylose during the second stage of a two-stage propagation.

FIG. 13B is a line graph showing the growth of ethanologen using xylose during the second stage of a two-stage propagation.

FIG. **14**A is a line graph showing the growth of ethanologen using an initial loading of xylose during the second stage of a two-stage propagation.

FIG. 14B is a line graph showing the growth of ethanologen using a continuous xylose feed during the second stage of a two-stage propagation.

FIG. **15**A is a line graph showing xylose consumption and ethanol production by ethanologen both with and without aeration.

FIG. **15**B is a line graph showing the growth of ethanologen both with and without aeration.

FIG. **16A** is a graph showing the growth of ethanologen using xylose.

FIG. **16**B is a graph showing growth of ethanologen using xylose.

 $\ensuremath{\mathsf{FIG}}.16\ensuremath{\mathsf{C}}$ is a graph showing growth of ethanologen using glucose.

TABLES 1A and 1B list the composition of biomass comprising lignocellulosic plant material from the corn plant according to exemplary and representative embodiments.

TABLES 2A and 2B list the composition of the liquid component of pre-treated biomass according to exemplary and representative embodiments.

TABLES 3A and 3B list the composition of the solids component of pre-treated biomass according to exemplary and representative embodiments.

TABLE 4 lists the growth medium composition according to Examples 1A through Example 4.

TABLES 5A and 5B list the results of use of a system according to Example 1A.

TABLES 6A and 6B list the results of use of a system according to Example 1B.

TABLES 7A, 7B and 7C list the results of use of a system according to Example 2.

TABLES 8A and 8B list the results of use of a system according to Example 3.

TABLES 9A and 9B list the results of use of a system according to Example 4.

TABLES 10A and 10B list the results of use of a system according to Example 5.

TABLES 11A through 11C list the results of use of a system according to Example 6.

DETAILED DESCRIPTION

Referring to FIG. 1A, a biorefinery configured to produce ethanol from biomass is shown.

According to an exemplary embodiment, the biorefinery is configured to produce ethanol from biomass in the form of a lignocellulosic feedstock such as plant material from the corn plant (e.g. corn cobs and corn stover). Lignocellulosic feedstock such as lignocellulosic material from the corn plant comprises cellulose (from which C6 sugars such as glucose can be made available) and/or hemicellulose (from which C5 sugars such as xylose and arabinose can be made available). 15

As shown in FIG. 1A, the biorefinery comprises an area where biomass is delivered and prepared to be supplied to the cellulosic ethanol production facility. The cellulosic ethanol production facility comprises apparatus for preparation, pretreatment and treatment of the biomass into treated biomass 20 suitable for fermentation into fermentation product in a fermentation system. The facility comprises a distillation system in which the fermentation product is distilled and dehydrated into ethanol. As shown in FIG. 1A, the biorefinery may also comprise a waste treatment system (shown as comprising an 25 anaerobic digester and a generator). According to other alternative embodiments, the waste treatment system may comprise other equipment configured to treat, process and recover components from the cellulosic ethanol production process, such as a solid/waste fuel boiler, anaerobic digester, aerobic 30 digester or other biochemical or chemical reactors.

As shown in FIG. 1B, according to an exemplary embodiment, a biorefinery may comprise a cellulosic ethanol production facility (which produces ethanol from lignocellulosic material and components of the corn plant) co-located with a 35 corn-based ethanol production facility (which produces ethanol from starch contained in the endosperm component of the corn kernel). As indicated in FIG. 1B, by co-locating the two ethanol production facilities, certain plant systems may be shared, for example, systems for dehydration, storage, dena- 40 turing and transportation of ethanol, energy/fuel-to-energy generation systems, plant management and control systems, and other systems. Corn fiber (a component of the corn kernel), which can be made available when the corn kernel is prepared for milling (e.g. by fractionation) in the corn-based 45 ethanol production facility, may be supplied to the cellulosic ethanol production facility as a feedstock. Fuel or energy sources such as methane or lignin from the cellulosic ethanol production facility may be used to supply power to either or both co-located facilities. According to other alternative 50 embodiments, a biorefinery (e.g. a cellulosic ethanol production facility) may be co-located with other types of plants and facilities, for example an electric power plant, a waste treatment facility, a lumber mill, a paper plant or a facility that processes agricultural products.

Referring to FIG. 2, a system for preparation of biomass delivered to the biorefinery is shown. The biomass preparation system may comprise apparatus for receipt/unloading of the biomass, cleaning (i.e. removal of foreign matter), grinding (i.e. milling, reduction or densification), and transport and conveyance for processing at the plant. According to an exemplary embodiment, biomass in the form of corn cobs and stover may be delivered to the biorefinery and stored (e.g. in bales, piles or bins, etc.) and managed for use at the facility. According to a preferred embodiment, the biomass may comprise at least 20 to 30 percent corn cobs (by weight) with corn stover and other matter. According to other exemplary

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embodiments, the preparation system of the biorefinery may be configured to prepare any of a wide variety of types of biomass (i.e. plant material) for treatment and processing into ethanol and other bioproducts at the plant.

Referring to FIG. 3, a schematic diagram of the cellulosic ethanol production facility is shown. According to a preferred embodiment, biomass comprising plant material from the corn plant is prepared and cleaned at a preparation system. After preparation, the biomass is mixed with water into a slurry and is pre-treated at a pre-treatment system. In the pre-treatment system, the biomass is broken down (e.g. by hydrolysis) to facilitate separation into a liquid component (e.g. a stream comprising the C5 sugars) and a solids component (e.g. a stream comprising cellulose from which the C6 sugars can be made available). The C5-sugar-containing liquid component (C5 stream) and C6-sugar-containing solids component (C6 stream) can be treated (as may be suitable) and fermented in a fermentation system. Fermentation product from the fermentation system is supplied to a distillation system where the ethanol is recovered.

As shown in FIGS. 3 and 4A, removed components from treatment of the C5 stream can be treated or processed to recover by-products, such as organic acids and furfural. As shown in FIGS. 3 and 4B, removed components from treatment of the C6 stream, such as lignin or other components, can be treated or processed into bioproducts or into fuel (such as lignin for a solid fuel boiler or methane produced by treatment of residual/removed matter such as acids and lignin in an anaerobic digester). As shown in FIGS. 4A, 4B and 4C, components removed during treatment and production of ethanol from the biomass from either or both the C5 stream and the C6 stream (or at distillation) may be processed into bioproducts (e.g. by-products or co-products) or recovered for use or reuse. As shown in FIG. 4C, removed components from the distillation system (such as stillage or removed solids) or from the treatment of the fermentation product before distillation (e.g. removed solids and particulate matter, which may comprise residual lignin, etc.) can be treated or processed into bioproducts or fuel (e.g. methane produced in an anerobic digester).

According to a preferred embodiment, the biomass comprises plant material from the corn plant, such as corn cobs, husks and leaves and stalks; the composition of the plant material (i.e. cellulose, hemicellulose and lignin) will be approximately as indicated in TABLES 1A and 1B. According to a preferred embodiment, the plant material comprises corn cobs, husks/leaves and stalks (i.e. after cleaning/removal of foreign matter); for example, the plant material may comprise (by weight) up to 100 percent cobs, up to 100 percent husks/leaves, approximately 50 percent cobs and approximately 50 percent husks/leaves, approximately 30 percent cobs and approximately 50 percent husks/leaves and approximately 20 percent stalks, or any other combinations of cobs, husks/leaves and stalks from the corn plant. See TABLE 1A. 55 According to an exemplary embodiment, corn stalks comprise the upper half or three-quarters portion of the stalk. According to an alternative embodiment, the lignocellulosic plant material may comprise fiber from the corn kernel (e.g. in some combination with other plant material). TABLE 1B provides typical and expected ranges believed to be representative of the composition of biomass comprising lignocellulosic material from the corn plant. According to exemplary embodiments, the lignocellulosic plant material of the biomass (from the corn plant) will comprise (by weight) cellulose at about 30 to 55 percent, hemicellulose at about 20 to 50 percent, and lignin at about 10 to 25 percent; according to a particularly preferred embodiment, the lignocellulosic plant

material of the biomass (cobs, husks/leaves and stalk portions from the corn plant) will comprise (by weight) cellulose at about 35 to 45 percent, hemicellulose at about 24 to 42 percent, and lignin at about 12 to 20 percent. According to a particularly preferred embodiment, pre-treatment of the biomass will yield a liquid component that comprises (by weight) xylose at no less than 1.0 percent and a solids component that comprises (by weight) cellulose (from which glucose can be made available) at no less than 45 percent.

Referring to FIGS. 5A and 5B, exemplary embodiments of 10 systems for the production of ethanol from biomass are shown. As shown in FIGS. 5A and 5B, biomass is pre-treated in a pre-treatment system and then separated into a liquid component and a solids component.

According to a preferred embodiment, in the pre-treatment 15 system an acid will be applied to the prepared biomass to facilitate the break down of the biomass for separation into the liquid component (C5 stream from which fermentable C5 sugars can be recovered) and the solids component (C6 stream from which fermentable C6 sugars can be accessed). 20 According to a preferred embodiment, the acid can be applied to the biomass in a reaction vessel under determined operating conditions (i.e. acid concentration, pH, temperature, time, pressure, solids loading, flow rate, supply of process water or steam, etc.) and the biomass can be agitated/mixed in the 25 reaction vessel to facilitate the break down of the biomass. According to exemplary embodiments, an acid such as sulfuric acid, hydrochloric acid, nitric acid, phosphoric acid, acetic acid, etc. (or a formulation/mixture of acids) can be applied to the biomass. According to a particularly preferred 30 embodiment, sulfuric acid will be applied to the biomass in pre-treatment.

The liquid component (C5 stream) comprises water, dissolved sugars (such as xylose, arabinose and glucose) to be made available for fermentation into ethanol, acids and other 35 soluble components recovered from the hemicellulose. (TABLE 2B provides typical and expected ranges believed to be representative of the composition of biomass comprising lignocellulosic material from the corn plant.) According to an exemplary embodiment, the liquid component may comprise 40 approximately 5 to 7 percent solids (i.e. suspended/residual solids such as partially-hydrolyzed hemicellulose, cellulose and lignin). According to a particularly preferred embodiment, the liquid component will comprise at least 2 to 4 percent xylose (by weight); according to other exemplary 45 embodiments, the liquid component will comprise no less than 1 to 2 percent xylose (by weight). TABLES 2A and 2B list the composition of the liquid component of pre-treated biomass (from prepared biomass as indicated in TABLES 1A and 1B) according to exemplary and representative embodi- 50

The solids component (C6 stream) comprises water, acids and solids such as cellulose from which sugar, such as glucose, can be made available for fermentation into ethanol, and lignin. (TABLE 3B provides typical and expected ranges 55 believed to be representative of the composition of biomass comprising lignocellulosic material from the corn plant.) According to an exemplary embodiment, the solids component may comprise approximately 10 to 40 percent solids (by weight) (after separation); according to a particularly pre- 60 ferred embodiment, the solids component will comprise approximately 20 to 30 percent solids (by weight). According to a preferred embodiment, the solids in the solids component comprise no less than 30 percent cellulose and the solids component may also comprise other dissolved sugars (e.g. glucose and xylose). TABLES 3A and 3B list the composition of the solids component of pre-treated biomass (from pre8

pared biomass as indicated in TABLES 1A and 1B) according to exemplary and representative embodiments.

During pre-treatment, the severity of operating conditions (such as pH, temperature and time) may cause formation of components that are inhibitory to fermentation. For example, under some conditions, the dehydration of C5 sugars (such as xylose or arabinose) may cause the formation of furfural and/or hydroxymethylfurfural (HMF). Acetic acid may also be formed, for example when acetate is released during the break down of cellulose in pre-treatment. Sulfuric acid, which may be added to prepared biomass to facilitate pre-treatment, if not removed or neutralized, may also be inhibitory to fermentation. According to an exemplary embodiment, by adjusting pre-treatment conditions (such as pH, temperature and time), the formation of inhibitors can be reduced or managed; according to other exemplary embodiments, components of the pre-treated biomass may be given further treatment to remove or reduce the level of inhibitors (or other undesirable matter).

Referring to FIGS. 5A and 5E, after pre-treatment and separation the C5 stream and the C6 stream are processed separately; as shown, the C5 stream and the C6 stream may be processed separately prior to co-fermentation (C5/C6 fermentation as shown in FIG. 5A) or processed separately including separate fermentation (separate C5 fermentation and C6 fermentation as shown in FIG. 5B).

Treatment of the C5 stream (liquid component) of the biomass may be performed in an effort to remove components that are inhibitory to efficient fermentation (e.g. furfural, HMF, sulfuric acid and acetic acid) and residual lignin (or other matter) that may not be fermentable from the C5 sugar component so that the sugars (e.g. xylose, arabinose, as well as other sugars such as glucose) are available for fermentation. The C5 sugars in the C5 stream may also be concentrated to improve the efficiency of fermentation (e.g. to improve the titer of ethanol for distillation).

Treatment of the C6 stream (solids component) of the biomass may be performed to make the C6 sugars available for fermentation. According to a preferred embodiment, hydrolysis (such as enzyme hydrolysis) may be performed to access the C6 sugars in the cellulose; treatment may also be performed in an effort to remove lignin and other non-fermentable components in the C6 stream (or to remove components such as residual acid or acids that may be inhibitory to efficient fermentation).

According to an exemplary embodiment shown in FIG. 5A, after pre-treatment and separation the C5 stream and the C6 stream can be treated separately and subsequently combined after treatment (e.g. as a slurry) for co-fermentation in the fermentation system to produce a C5/C6 fermentation product from the available sugars (e.g. xylose and glucose); the C5/C6 fermentation product can (after treatment, if any) be supplied to the distillation system for recovery of the ethanol (e.g. through distillation and dehydration). According to an exemplary embodiment shown in FIG. 5B, the C5 stream and the C6 stream can each be separately processed through fermentation and distillation (after treatment, if any) to produce ethanol. According to any preferred embodiment, a suitable fermenting organism (ethanologen) will be used in the fermentation system; the selection of an ethanologen may be based on various considerations, such as the predominant types of sugars present in the slurry. Dehydration and/or denaturing of the ethanol produced from the C5 stream and the CG stream may be performed either separately or in combination.

FIGS. 6A and 6B show the apparatus used for preparation, pre-treatment and separation of lignocellulosic biomass

according to an exemplary embodiment. As shown, biomass is prepared in a grinder (e.g. grinder or other suitable apparatus or mill). Pre-treatment of the prepared biomass is performed in a reaction vessel (or set of reaction vessels) supplied with prepared biomass and acid/water in a predetermined concentration (or pH) and other operating conditions. As shown in FIG. 6B, the pre-treated biomass can be separated in a centrifuge into a liquid component (C5 stream comprising primarily liquids with some solids) and a solids component (C6 stream comprising liquids and solids such as lignin and cellulose from which glucose can be made available by further treatment).

As shown in FIGS. 7A and 7B, a liquid component (C5 stream) is introduced to a treatment system. In the treatment system, the C5 stream may be treated by filtration and/or by concentration into a treated liquid component that comprises sugars available for fermentation. The treated liquid component is supplied to a fermentation system to produce by fermentation of the sugars with an ethanologen (i.e. an organism such as yeast) a fermentation product (that comprises ethanol).

According to a preferred embodiment, the ethanologen comprises a yeast derived from genetically modified recombinant Saccharomyces cerevisiae. According to a particularly preferred embodiment, the ethanologen is a strain of Saccharomyces cerevisiae yeast altered to convert xylose and glucose to ethanol (a genetically modified yeast derived from an organism as described in U.S. Pat. No. 7,622,284, assigned to Royal Nedalco B.V.).

Referring to FIG. 7B, a propagation system is provided for the ethanologen (shown as yeast). In the propagation system, yeast is supplied with a growth medium (e.g. water and a carbon source, such as sugar) and an agent (e.g. nutrients, etc.) to facilitate the growth of a sufficient amount of yeast (i.e. yeast cell mass) for inoculation (i.e. yeast inoculum to be supplied) to the fermentation system.

According to an exemplary embodiment the growth medium for the propagation system will comprise, for example, a sterile yeast extract-peptone medium, xylose as the carbon source, and other agents (e.g. nutrients). Agents supplied with the ethanologen may include antibiotics, supplemental or accessory enzymes, nutrients or other components providing nutritional or other benefits to the organism. Nutrients may comprise yeast extract, urea, diammonium phosphate, magnesium sulfate, zinc sulfate or other salts, etc. According to an exemplary embodiment, the yeast 45 inoculum is incubated under conditions comprising a temperature of about 30 degrees Celsius and a pH of about 5.5 for about 17 hours. According to alternative embodiments, to grow (inoculate) the yeast in the propagation system the temperature may be maintained in a range of about 28 to 32 50 degrees Celsius and the pH in a range of about 5.2 to 5.8 for a time of at least 12 hours.

Referring to FIGS. 7C and 9, an exemplary embodiment of the propagation system for the ethanologen (shown as yeast) employing two stages is shown. As shown in FIG. 9, a yeast culture can be grown into an initial yeast inoculum that can be provided to the first stage of the propagation system.

In the first propagation stage, the initial yeast inoculum is transferred to a larger vessel and diluted (e.g. by 250×). In the vessel, the initial yeast inoculum and a portion of the C5 stream (i.e. liquid component comprising C5/other sugars) and water may be supplied along with agents (such as nutrients) and fresh yeast. According to a preferred embodiment, yeast is grown in the first propagation stage under conditions comprising a temperature of about 30 degrees Celsius and a pH of about 5.5 for about 24 hours. According to other exemplary embodiments, the temperature may be maintained in a range of about 26 to 37 degrees and the pH in a range of about

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3.5 to 6.5 for a time of at least 24 hours. In the second propagation stage, the yeast inoculum from the first propagation stage is transferred to a larger vessel and diluted (e.g. by 10×). In the vessel, the yeast inoculum from the first propagation stage and a portion of the C5 stream (i.e. liquid component comprising C5/other sugars) and water may be supplied along with agents (such as nutrients) and fresh yeast. According to a preferred embodiment, yeast is grown in the second propagation stage under conditions comprising a temperature of about 30 degrees Celsius and a pH of about 5.5 for about 24 hours. According to other exemplary embodiments, the temperature may be maintained in a range of about 26 to 37 degrees and the pH in a range of about 3.5 to 6.5 for a time of at least 24 hours.

The fermentation product (which may also be referred to as beer or fermentation broth or as comprising beer or fermentation broth) will comprise ethanol and water as well as unfermented matter (e.g. any unfermented sugars) and non-fermentable matter (e.g. residual lignin and other solids). The fermentation product will also comprise in the form of particulate matter the ethanologen (i.e. yeast cells) that was used to produce ethanol as well as other components produced by the fermentation system, for example, such as glycerol (a product of fermentation) and acetic acid.

As shown in FIGS. 8A and 8E, according to an exemplary embodiment, a treatment system for the fermentation product may also be provided. The treatment system can comprise separation of the fermentation product into a liquid component (i.e. a treated fermentation product, which will comprise substantially ethanol and water) and a solids component (which will comprise substantially solids matter such as the ethanologen/yeast cells). According to a preferred embodiment, as shown in FIG. 8B, the separation of the fermentation product into the liquid component and solids component can be performed on a centrifuge. As shown in FIG. 8B, the solids component from treatment comprising the yeast cells can be supplied to and re-used in the fermentation system (i.e. recycled for use in a fermentation tank) along with additional or fresh yeast cells (if necessary). The yeast cells may be treated in a yeast cell treatment system. The yeast cell treatment system may comprise washing the yeast cells and separating the yeast cells prior to recirculation to a fermentation tank or the fermentation product stream.

According to any preferred embodiment, the yeast propagation system will provide for the growth of yeast into a suitable yeast cell mass at a suitable rate to be supplied to the fermentation system. According to a preferred embodiment, the system will allow for the growth of yeast using xylose as a carbon source for growth. According to a particularly preferred embodiment, the system will allow for the selective growth of yeast that can use xylose as a carbon source (i.e. yeast that will propagate in a medium comprising xylose) even if other yeast is present (i.e. as a contaminant); in a medium that provides xylose as a sole carbon source (i.e. a medium that does not contain substantial amounts of glucose), yeast that are capable of propagating using, xylose as a carbon source will propagate and other/contaminant yeast that may not be as capable of propagating using xylose as a carbon source (such as more common forms of yeast that typically propagate in a medium containing glucose) will not propagate at the same rate (or at all). According to a particularly preferred embodiment, the yeast will be capable of, fermenting both xylose and glucose into ethanol. According to a preferred embodiment, the yeast propagation system will provide a growth medium and environment in which the yeast will convert sugar (e.g. xylose) into yeast cell mass rather than ethanol, for example, under conditions such as aeration (see FIGS. 15A and 15B) or will allow the yeast to withstand higher concentrations of sugar (e.g. xylose) during propagation (see FIGS. 16A and 16B). According to any preferred

embodiment, the system will facilitate the efficient growth of yeast cell mass into an inoculum that can be provided to the fermentation system in a biorefinery. According to a particularly preferred embodiment the yeast cell mass will grow by about 200 to 500 fold in the first stage and about 20 to 40 fold in the second stage.

* * *

A series of Examples were conducted according to exemplary embodiments of the yeast propagation system (as shown, for example, in FIGS. 7B, 7C and 9) to evaluate ethanologen growth under various conditions. The ethanologen used in the Examples was a strain of Saccharomyces cerevisiae yeast able to convert xylose and glucose to ethanol (a genetically modified yeast derived from an organism as described in U.S. Pat. No. 7,622,284, by Royal Nedalco B.V., for example, Strain No. RWB218; Strain No. RN1001; and Strain No. RN1014). Data from the Examples is shown in FIGS. 10A through 16C and TABLES 5A through 11C. TABLE 4 lists the composition of the growth medium (including added agents such as nutrients) according to Examples 1A through 4.

An ethanologen culture was grown into an initial inoculum (yeast inoculum) using a sterile yeast extract-peptone (YP) medium (with 12.5 grams yeast extract per liter of medium and 10 grams peptone per liter). The inoculum was incubated at 30 degrees Celsius for approximately 17 to 18 hours. An inoculum to media ratio of 1:250 was used. A pump was used to control the xylose feed rate. The pH of the medium was able to be maintained at 5.5 (by adding a 45 percent by weight solution of potassium hydroxide). The samples were periodically analyzed for yeast growth (cell mass), sugars, organic acids and ethanol. The optical density was measured (at 600 nanometers using a spectrophotometer) as an indication of the amount (i.e. cell mass) of yeast in the sample. (HPLC was used to analyze other components.)

EXAMPLE 1A

The propagation system was used in Example 1A to evaluate the effect of pH regulation on the growth of the ethanologen. The ethanologen was yeast (Strain No. RN1001). Samples were prepared in two separate reaction vessels. The samples comprised a medium (e.g. water and agents, such as nutrients, as indicated in TABLE 4) and the yeast inoculum. The samples also comprised xylose at a concentration of 30 grams per liter (of medium). The pH of the samples in each 45 reaction vessel was adjusted to 5.5. The temperature of each reaction vessel was held at 30 degrees Celsius. The yeast was propagated in each reaction vessel for 54 hours. In one of the reaction vessels, the pH was maintained (regulated) at 5.5; in the other reaction vessel the pH was unregulated. After 54 hours xylose solution (50 percent by weight) and additional nutrients were added resulting in a total amount of xylose of about 60 grams/liter. The propagation of the yeast continued for another 66 hours. In one of the reaction vessels, the pH was maintained (regulated) at 5.5; in the other reaction vessel the pH was unregulated. The samples were tested and analyzed for yeast growth (by dry weight), ethanol concentration, xylose concentration and optical density (OD_{600}) to evaluate xylose conversion. It was observed that the sample in which the pH was maintained at 5.5 produced more yeast than the sample in which pH was unregulated (within the indicated 60 operating conditions). The results are shown in FIGS. 10A and 10B and TABLES 5A and 5B.

EXAMPLE 1B

The propagation system was used in Example 1B to evaluate the effect of feeding xylose at different rates on the growth

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of the ethanologen. The ethanologen was yeast (Strain No. RN1001). Samples were prepared in two separate reaction vessels. The samples comprised a medium (e.g. water and agents, such as nutrients, as indicated in TABLE 4) and the yeast inoculum. The samples also comprised xylose at a concentration of 20 grams per liter (of medium). The temperature of each reaction vessel was held at 30 degrees Celsius. The yeast was propagated in each reaction vessel for 24 hours. After 24 hours xylose solution (50 percent by weight, along with additional nutrients) was fed into one reaction vessel at 0.14 milliliters per minute for 46 hours resulting in a total xylose addition of 90 grams per liter, and into the other reaction vessel at 0.28 milliliters per minute for 46 hours resulting in a total amount of xylose of about 100 grams per liter. The propagation of the yeast continued for another 50 hours. The samples were tested and analyzed for yeast growth (by dry weight), ethanol concentration, xylose concentration and optical density (OD_{600}) to evaluate xylose conversion. It was observed that the samples exhibited similar yeast growth rates regardless of the rate of addition of xylose into the samples, (within the indicated operating conditions). The results are shown in FIGS. 11A and 11B and TABLES 6A and

EXAMPLE 2

The propagation system was used in Example 2 to evaluate the effect of different sources of xylose on the growth of the ethanologen. A first biomass liquid component was prepared by dilute acid pre-treatment of corn cobs (see FIG. 6A and TABLES 2A and 2B). A treated biomass liquid component was prepared by treating the first liquid component by ion exchange chromatography. The ethanologen was yeast (Strain No. RN1001). Samples were prepared in three separate reaction vessels. The samples comprised a medium (e.g. water and agents, such as nutrients, as indicated in TABLE 4) and the yeast inoculum. The samples also comprised xylose at a concentration of 20 grams per liter (of medium). The pH of each sample was adjusted to and maintained (regulated) at 5.5. The temperature of each reaction vessel was held at 30 degrees Celsius. The yeast was propagated in each reaction vessel for 24 hours. After 24 hours the sample in the first reaction vessel was supplied with xylose solution (50 percent by weight, along with additional nutrients) at 0.19 milliliters per minute for 30 hours resulting in a total amount of xylose of about 106 grams per liter. The propagation of the yeast continued for another 66 hours. After 24 hours the sample in the second reaction vessel was supplied with xylose solution (50 percent by weight, along with additional nutrients) at 0.26 milliliters per minute for about 22 hours and after that with the biomass liquid component at 2.8 milliliters per minute for about 2.6 hours resulting in a total amount of xylose of about 95 grams per liter. The propagation of the yeast continued for another 71 hours. After 24 hours the sample in the third reaction vessel was supplied with xylose solution (50 percent by weight, along with additional nutrients) at 0.19 milliliters per minute for about 22 hours and after that with the treated biomass liquid component at 3.0 milliliters per minute for about 2 hours resulting in a total amount of xylose of about 92 grams per liter. The propagation of the yeast continued for another 72 hours. The samples were tested and analyzed for yeast growth (by dry weight), ethanol concentration, xylose concentration and optical density (at 600 nanometers $[\mathrm{OD}_{600}])$ to evaluate xylose conversion. It was observed that xylose obtained from biomass (lignocellulosic plant material) could be used to propagate yeast (within the indicated operating conditions). The results are shown in FIGS. 12A through 12C and TABLES 7A through 7C.

EXAMPLE 3

The propagation system as indicated in FIGS. 7C and 9 was used in Example 3 to evaluate the growth of the ethanologen

in a two-stage propagation system with differing xylose levels. The ethanologen was yeast (Strain No. RN1001). In the first stage a sample was prepared in a reaction vessel. The sample comprised medium (e.g. water and agents, such as nutrients, as indicated in TABLE 4) and the yeast inoculum. 5 The sample also comprised xylose at a concentration of 20 grams per liter (of medium). The yeast was propagated for 24 hours. After 24 hours 300 mL of the sample from the first stage was used to inoculate each of two samples in two separate reaction vessels (stage two). The samples comprised 10 medium (e.g. water and agents, such as nutrients, as indicated in TABLE 4) so that the total sample volume was 3 liters in each reaction vessel of the second stage. The sample in the first vessel of the second stage comprised xylose at a concentration of 40 grams per liter (of medium), and the sample in the second vessel of the second stage comprised xylose at a concentration of 30 grams per liter (of medium). The temperature of each reaction vessel was held at 30 degrees Celsius. The yeast was propagated in each reaction vessel for 12 hours. The pH of each sample was adjusted to and maintained (regulated) at 5.5. After 12 hours the sample in the first reaction vessel of the second stage was supplied with xylose solution (50 percent by weight, along with additional nutrients) at 0.26 milliliters per minute for 12 hours resulting in a total amount of xylose of about 64 grams per liter. The propagation of the yeast continued for another 30 hours. After 12 25 hours the sample in the second reaction vessel of the second stage was supplied with xylose solution (50 percent by weight, along with additional nutrients) at 0.30 milliliters per minute for about 12 hours resulting in a total amount of xylose of about 64 grams per liter. The propagation of the yeast 30 continued for another 30 hours. It was observed that the total time to propagate yeast (e.g. yeast cell mass grown from approximately 0.04 grams to 20 grams in the first stage and from approximately 2 grams to 75 grams in the second stage) could be reduced in a two-stage propagation system (i.e. 35 using approximately 78 hours) as compared to a one-stage propagation system (i.e. using approximately 100 to 120 hours). See also Examples 1A, 1B and 2. The results are shown in FIGS. 13A and 13B and TABLES 8A and 8B.

EXAMPLE 4

The propagation system as indicated in FIGS. 7C and 9 was used in Example 4 to evaluate the effect of xylose feeding on the growth of the ethanologen. The ethanologen was yeast (Strain No. RN1014). In the first stage a sample was prepared 45 in a reaction vessel. The sample comprised medium (e.g. water and agents, such as nutrients, as indicated in TABLE 4) and the yeast inoculum. The sample also comprised xylose at a concentration of 20 grams per liter (of medium). The yeast was propagated for 24 hours. After 24 hours 300 mL of the 50 sample from the first stage was used to inoculate each of two samples in two separate reaction vessels (stage two). The samples comprised medium (e.g. water and agents, such as nutrients, as indicated in TABLE 4) so that the total sample volume was 3 liters in each reaction vessel of the second stage. Both samples of the second stage comprised xylose at a concentration of 35 grams per liter (of medium). The temperature of each reaction vessel was held at 30 degrees Celsius. The yeast was propagated in each reaction vessel for 23 hours. The pH of each sample was adjusted to and maintained (regulated) at 5.5. After 23 hours the sample in the first reaction vessel of the second stage was supplied with a single dose of xylose solution (50 percent by weight, along with additional nutrients) resulting in a total amount of xylose of about 64 grams per liter. The propagation of the yeast continued for another 31 hours. After 23 hours the sample in the second 65 reaction vessel of the second stage was supplied with xylose solution (50 percent by weight, along with additional nutri14

ents) at 0.31 milliliters per minute for about 8.2 hours resulting in a total amount of xylose of about 64 grams per liter. The propagation of the yeast continued for about another 32 hours. It was observed that the growth of yeast could be improved when additional xylose was supplied to the sample (i.e. after 23 hours) on a continuously-fed basis rather than in a single dose (within the indicated operating conditions). The results are shown in FIGS. **14**A and **14**B and TABLES 9A and on

EXAMPLE 5

The propagation system was used in Example 5 to evaluate the effect of aeration on the growth of the ethanologen. The ethanologen was yeast (Strain No. RWB218). Samples were prepared in two separate reaction vessels: The samples comprised medium (e.g. water and agents, such as nutrients, as indicated in TABLE 4) and the yeast inoculum. The samples also comprised xylose at a concentration of 30 grams per liter (of medium). One reaction vessel was aerated at 5 liters per minute; the other reaction vessel was not aerated. The yeast was propagated in each reaction vessel at 32 degrees Celsius for 53 hours. The samples were tested and analyzed for yeast growth (by dry weight), ethanol concentration, xylose concentration and optical density (OD₆₀₀) to evaluate xylose conversion. It was observed that the growth of yeast could be improved when the sample was aerated (within the indicated operating conditions) insofar as the yeast used the supplied xylose for cell mass growth rather than for the production of ethanol. The results are shown in FIGS. 15A and 15B and TABLES 10A and 10B.

EXAMPLE 6

The propagation system was used in Example 6 to evaluate the effect of xylose and glucose concentrations on the growth of the ethanologen. The ethanologen was yeast (Strain No. RWB218). Samples were prepared in three separate reaction vessels. The samples comprised medium (e.g. water and agents, such as nutrients, as indicated in TABLE 11A) and the yeast inoculum. The temperature of each reaction vessel was held at 32 degrees Celsius. Each reaction vessel was aerated at 4.5 liters per minute. The first and second reaction vessels were supplied with xylose at a concentration of 60 grams per liter; the third reaction vessel was supplied with glucose at a concentration of 60 grams per liter. The pH of the samples in the second and third reaction vessels was adjusted to and maintained (regulated) at 5.5. The yeast was propagated in the first and second reaction vessel at 32 degrees Celsius for 120 hours. The yeast was propagated in the third reaction vessel at 32 degrees Celsius for 52 hours. It was observed that the growth of yeast could be improved when the sample was aerated insofar as the yeast used the supplied xylose for cell mass growth rather than the production of ethanol, notwithstanding the concentration of xylose (within the indicated operating conditions). The results are shown in FIGS. 16A through 16C and TABLES 11A through 11C.

* * *

The embodiments as disclosed and described in the application (including the FIGURES and Examples) are intended to be illustrative and explanatory of the present inventions. Modifications and variations of the disclosed embodiments, for example, of the apparatus and processes employed (or to be employed) as well as of the compositions and treatments used (or to be used), are possible; all such modifications and variations are intended to be within the scope of the present inventions.

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TABLE 1A

	Biomass Composition									
	Husks/		Cellulose		Hemico	ellulose				
Cob (percent)	Leaves (percent)	Stalk (percent)	(Glucan) (percent)	Xylan (percent)	Arabinan (percent)	Acetate (percent)	Composite (percent)	Lignin (percent)	Ash (percent)	
100	0	0	36.0	33.3	3.6	3.0	39.9	14.9	2.2	
0	100	0	37.2	25.6	4.9	2.2	32.7	13.0	7.7	
0	0	100	41.7	22.5	2.4	2.6	27.5	18.3	3.7	
50	0	50	38.8	27.9	3.0	2.8	33.7	16.6	3.0	
50	50	0	36.6	29.5	4.2	2.6	36.3	14.0	5.0	
30	50	20	37.7	27.3	4.0	2.5	33.8	14.6	5.3	

	7	TABLE 1B			15		-	TABLE 3B		
	Typical and	Biomass d Expected Compo	sition				So	Treated Biomass lids Component d Expected Compo	eition	
	Cellulose (Glucan) (percent) (approx.)	Hemicellulose (percent) (approx.)	Lignin (percent) (approx.)	Ash (percent) (approx.)	20		Cellulose (Glucan) (percent) (approx.)	Hemicellulose (percent) (approx.)	Lignin (percent) (approx.)	Ash (percent) (approx.)
Typical Range Expected Range	35-45 30-55	24-42 20-50	12-20 10-25	2-8 1-10	25	Typical Range Expected Range	48-62 45-65	8-17 5-20	22-30 20-32	1-10 1-10

TABLE 2A

			reated Biom			
Cob (percent)	Husks/Leaves (percent)	Stalk (percent)	Glucose (percent)	Xylose (percent)	Arabinose (percent)	Acetic Acid (ppm)
100	0	0	0.4	4.8	0.6	6090
0	100	0	0.4	2.7	0.5	3400
0	0	100	0.4	4.2	0.4	6180
50	0	50	0.4	4.5	0.4	6135
30	50	20	0.4	3.6	0.5	4763

TABLE 2B TABLE 4

		eated Biomas id Component				Growth Medium Comp	osition
		Expected Com Xylose		Acetic Acid	45	Component	Concentration*
	(percent) (approx.)	(percent) (approx.)	(percent) (approx.)	(ppm) (approx.)	_	Yeast Extract	5 g/L
Typical Range Expected Range	0-1 0-1	2-6 1-8	0-1 0-1	3000-6400 2000-8000	50	Urea Diammonium Phosphate	10 g/L 2.5 g/L
						Magnesium Sulfate Heptahydrate	0.5 g/L

TABLE 3A

	Pre-Treated Biomass Solids Component Composition								
	Husks/		Cellulose		Hemico	ellulose			
Cob (percent)	Leaves (percent)	Stalk (percent)	(Glucan) (percent)	Xylan (percent)	Arabinan (percent)	Acetate (percent)	Composite (percent)	Lignin (percent)	Ash (percent)
100	0	0	60.2	9.5	0.9	0.3	10.7	26.7	1.2
0	100	0	54.4	1.3	0.7	0.7	10.4	23.8	9.7
0	0	100	51.1	1.4	1.0	1.0	15.4	27.3	3.1
50	0	50	55.7	5.5	0.9	0.6	13.1	27.0	2.2
50	50	0	57.3	5.4	0.8	0.5	10.6	25.2	5.4
30	50	20	55.5	3.8	0.8	0.6	11.5	25.4	5.8

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TABLE 4-cc

18 TADIE 7A

	TABLE	4-continued				TA	BLE 7A	
	Growth Med	lium Composition					D "	37. 1
Component		(Concentration*	5	Time (h)	OD_{600}	Dry cell wt. (g/L)	Xylose (% w/v)
Zinc Sulfate Lactoside 2	Heptahydrate 17		0.02 g/L 5 PPM	_	0	0.0	NT	2.04
In Water				_	24	14.8	10.08	0.36
					30	22.3	NT	0.63
	TAI	BLE 5A		10	48	46.4	30.46	3.46
		Dry cell wt.	Xylose		54	48.4	NT	4.71
Time (h)	OD_{600}	(g/L)	(% w/v)		79	68.3	45.00	2.47
0	0.1	NT	3.16		102	65.4	51.91	1.38
24	16.5	10.78	1.18	15	120	78.9	58.40	0.78
30 48	26.6 28.2	NT 17.21	0.29 0.01		120	78.9	36.40	0.78
54	29.0	NT	3.06					
78	49.2	27.67	0.55		0 ₆₀₀ —Optical densit	y at 600 nm		
102 120	47.1 46.3	30.53 31.84	0.20 0.13		Mot tested			
		31.04	0.15					
D ₆₀₀ —Optical densit T—Not tested	y at 600 nm			_		TA	BLE 7B	
							Dry cell wt.	Xylose
	TAI	BLE 5B		25	Time (h)	OD_{600}	(g/L)	(% w/v)
Time (h)	OD_{600}	Dry cell wt. (g/L)	Xylose (% w/v)		0	0.1	NT	2.02
			(70 W/V)	_	24	14.9	9.97	0.31
0 24	0.1	NT	3.31		30	18.7	NT	0.70
30	12.4 15.6	7.23 NT	1.59 1.44	30	48	45.7	30.04	3.39
48	14.6	8.55	1.20		54	43.0	NT	0.46
54	19.7	NT	3.90		79	48.8	31.00	0.05
78 102	29.5 34.1	16.35 16.77	2.39 1.88		102	46.8	33.72	0.09
120	33.1	17.04	1.71	35	120	52.5	33.45	0.03
	v at 600 nm				O-411 dit	. 600		
	, 40 000 1111				O ₆₀₀ —Optical densit —Not tested	y at 600 nm		
D ₆₀₀ —Optical densit IT—Not tested		BLE 6A					.BLF 7 <i>C</i>	
		BLE 6A Dry cell wt. (g/L)	Xylose (% w/v)	N	—Not tested	TA	BLE 7C Dry cell wt.	Xylose
T—Not tested Time (h)	OD ₆₀₀ 0.2	Dry cell wt. (g/L)	(% w/v) 2.09	N	Time (h)	TA	Dry cell wt. (g/L)	(% w/v)
T—Not tested Time (h) 0 24	OD ₆₀₀ 0.2 11.0	Dry cell wt. (g/L) NT 6.52	(% w/v) 2.09 0.61	40	Time (h)	OD ₆₀₀	Dry cell wt. (g/L) NT	(% w/v) 2.02
T—Not tested Time (h)	OD ₆₀₀ 0.2	Dry cell wt. (g/L)	(% w/v) 2.09	N	Time (h)	TA	Dry cell wt. (g/L)	(% w/v)
Time (h) 0 24 30 48 54	OD ₆₀₀ 0.2 11.0 21.0 37.8 47.9	Dry cell wt. (g/L) NT 6.52 NT 21.88 NT	(% w/v) 2.09 0.61 0.38 1.29 1.62	40	Time (h) 0 24 30 48	OD ₆₀₀ 0.1 15.4 22.4 44.2	Dry cell wt. (g/L) NT 10.01 NT 27.85	(% w/v) 2.02 0.30 0.30 1.25
Time (h) 0 24 30 48 54 78	OD ₆₀₀ 0.2 11.0 21.0 37.8 47.9 64.3	Dry cell wt. (g/L) NT 6.52 NT 21.88 NT 34.06	(% w/v) 2.09 0.61 0.38 1.29 1.62 2.66	40	Time (h) 0 24 30 48 54	OD ₆₀₀ 0.1 15.4 22.4 44.2 43.1	Dry cell wt. (g/L) NT 10.01 NT 27.85 NT	(% w/v) 2.02 0.30 0.30 1.25 2.01
Time (h) 0 24 30 48 54	OD ₆₀₀ 0.2 11.0 21.0 37.8 47.9	Dry cell wt. (g/L) NT 6.52 NT 21.88 NT	(% w/v) 2.09 0.61 0.38 1.29 1.62	40	Time (h) 0 24 30 48	OD ₆₀₀ 0.1 15.4 22.4 44.2	Dry cell wt. (g/L) NT 10.01 NT 27.85	(% w/v) 2.02 0.30 0.30 1.25
Time (h) 0 24 30 48 54 78 102 120	OD ₆₀₀ 0.2 11.0 21.0 37.8 47.9 64.3 61.3 61.6	Dry cell wt. (g/L) NT 6.52 NT 21.88 NT 34.06 37.65	(% w/v) 2.09 0.61 0.38 1.29 1.62 2.66 1.24	40	Time (h) 0 24 30 48 54 79	OD ₆₀₀ 0.1 15.4 22.4 44.2 43.1 44.5	Dry cell wt. (g/L) NT 10.01 NT 27.85 NT 28.00	(% w/v) 2.02 0.30 0.30 1.25 2.01 0.32
Time (h) 0 24 30 48 54 78 102 120 D ₆₀₀ —Optical densit	OD ₆₀₀ 0.2 11.0 21.0 37.8 47.9 64.3 61.3 61.6	Dry cell wt. (g/L) NT 6.52 NT 21.88 NT 34.06 37.65	(% w/v) 2.09 0.61 0.38 1.29 1.62 2.66 1.24	40 45 50 OI	Time (h) 0 24 30 48 54 79 102	OD ₆₀₀ 0.1 15.4 22.4 44.2 43.1 44.5 40.5 46.8	Dry cell wt. (g/L) NT 10.01 NT 27.85 NT 28.00 30.99	(% w/v) 2.02 0.30 0.30 1.25 2.01 0.32 0.15
Time (h) 0 24 30 48 54 78 102	OD ₆₀₀ 0.2 11.0 21.0 37.8 47.9 64.3 61.3 61.6 y at 600 nm	Dry cell wt. (g/L) NT 6.52 NT 21.88 NT 34.06 37.65 40.64	(% w/v) 2.09 0.61 0.38 1.29 1.62 2.66 1.24	40 45 50 OI	Time (h) 0 24 30 48 54 79 102 120 0600—Optical densit	OD ₆₀₀ 0.1 15.4 22.4 44.2 43.1 44.5 40.5 46.8	Dry cell wt. (g/L) NT 10.01 NT 27.85 NT 28.00 30.99	(% w/v) 2.02 0.30 0.30 1.25 2.01 0.32 0.15
Time (h) 0 24 30 48 54 78 102 120	OD ₆₀₀ 0.2 11.0 21.0 37.8 47.9 64.3 61.3 61.6 y at 600 nm	Dry cell wt. (g/L) NT 6.52 NT 21.88 NT 34.06 37.65 40.64	(% w/v) 2.09 0.61 0.38 1.29 1.62 2.66 1.24 0.74	40 45 50 OI	Time (h) 0 24 30 48 54 79 102 120 0600—Optical densit	OD ₆₀₀ 0.1 15.4 22.4 44.2 43.1 44.5 40.5 46.8 y at 600 nm	Dry cell wt. (g/L) NT 10.01 NT 27.85 NT 28.00 30.99	(% w/v) 2.02 0.30 0.30 1.25 2.01 0.32 0.15
Time (h) 0 24 30 48 54 78 102 120 D600—Optical densit	OD ₆₀₀ 0.2 11.0 21.0 37.8 47.9 64.3 61.3 61.6 y at 600 nm	Dry cell wt. (g/L) NT 6.52 NT 21.88 NT 34.06 37.65 40.64 BLE 6B Dry cell wt. (g/L)	(% w/v) 2.09 0.61 0.38 1.29 1.62 2.66 1.24 0.74 Xylose (% w/v)	40 45 50 OI NO	Time (h) 0 24 30 48 54 79 102 120 0600—Optical densit	OD ₆₀₀ 0.1 15.4 22.4 44.2 43.1 44.5 40.5 46.8 y at 600 nm	Dry cell wt. (g/L) NT 10.01 NT 27.85 NT 28.00 30.99 32.29	(% w/v) 2.02 0.30 0.30 1.25 2.01 0.32 0.15
Time (h) 0 24 30 48 54 78 102 120 D ₆₀₀ —Optical densit T—Not tested Time (h)	OD ₆₀₀ 0.2 11.0 21.0 37.8 47.9 64.3 61.3 61.6 y at 600 nm TAI	Dry cell wt. (g/L) NT 6.52 NT 21.88 NT 34.06 37.65 40.64 BLE 6B Dry cell wt. (g/L) NT	(% w/v) 2.09 0.61 0.38 1.29 1.62 2.66 1.24 0.74 Xylose (% w/v) 2.13	40 45 50 OI NO	Time (h) 0 24 30 48 54 79 102 120 0600—Optical densit	OD ₆₀₀ 0.1 15.4 22.4 44.2 43.1 44.5 40.5 46.8 y at 600 nm	Dry cell wt. (g/L) NT 10.01 NT 27.85 NT 28.00 30.99 32.29 BLE 8A Dry cell wt. (g/L)	(% w/v) 2.02 0.30 0.30 1.25 2.01 0.32 0.15 0.04 Xylose (% w/v)
T—Not tested Time (h) 0 24 30 48 54 78 102 120 D ₆₀₀ —Optical densit T—Not tested	OD ₆₀₀ 0.2 11.0 21.0 37.8 47.9 64.3 61.3 61.6 y at 600 nm	Dry cell wt. (g/L) NT 6.52 NT 21.88 NT 34.06 37.65 40.64 BLE 6B Dry cell wt. (g/L)	(% w/v) 2.09 0.61 0.38 1.29 1.62 2.66 1.24 0.74 Xylose (% w/v)	40 — 40 — 45 — 50 — OI NO	Time (h) 0 24 30 48 54 79 102 120 0600—Optical densit	OD ₆₀₀ 0.1 15.4 22.4 44.2 43.1 44.5 40.5 46.8 y at 600 nm	Dry cell wt. (g/L) NT 10.01 NT 27.85 NT 28.00 30.99 32.29 BLE 8A Dry cell wt.	(% w/v) 2.02 0.30 0.30 1.25 2.01 0.32 0.15 0.04
Time (h) 0 24 30 48 54 78 102 120 D ₆₀₀ —Optical densit T—Not tested Time (h) 0 24 30 48	TAI OD ₆₀₀ 0.2 11.0 21.0 37.8 47.9 64.3 61.3 61.6 y at 600 nm TAI OD ₆₀₀ 0.1 12.0 22.2 42.9	Dry cell wt. (g/L) NT 6.52 NT 21.88 NT 34.06 37.65 40.64 BLE 6B Dry cell wt. (g/L) NT 6.92 NT 25.79	(% w/v) 2.09 0.61 0.38 1.29 1.62 2.66 1.24 0.74 Xylose (% w/v) 2.13 0.61 0.98 3.81	40 45 50 OI NO	Time (h) 0 24 30 48 54 79 102 120 0e00—Optical densite—Not tested Time (h) 0 6 12	OD ₆₀₀ 0.1 15.4 22.4 44.2 43.1 44.5 40.5 46.8 y at 600 nm TA OD ₆₀₀ 1.8 4.4 16.3	Dry cell wt. (g/L) NT 10.01 NT 27.85 NT 28.00 30.99 32.29 BLE 8A Dry cell wt. (g/L) NT NT NT	(% w/v) 2.02 0.30 0.30 1.25 2.01 0.32 0.15 0.04 Xylose (% w/v) 4.35 3.81 2.83
Time (h) 0 24 30 48 54 78 102 120 D ₆₀₀ —Optical densit T—Not tested Time (h) 0 24 30 48 54	OD ₆₀₀ 0.2 11.0 21.0 37.8 47.9 64.3 61.3 61.6 y at 600 nm TAI OD ₆₀₀ 0.1 12.0 22.2 42.9 47.7	Dry cell wt. (g/L) NT 6.52 NT 21.88 NT 34.06 37.65 40.64 BLE 6B Dry cell wt. (g/L) NT 6.92 NT 25.79 NT	(% w/v) 2.09 0.61 0.38 1.29 1.62 2.66 1.24 0.74 Xylose (% w/v) 2.13 0.61 0.98 3.81 4.92	40 — 40 — 45 — 50 — OI NO	Time (h) 0 24 30 48 54 79 102 120 0600—Optical densit	OD ₆₀₀ 0.1 15.4 22.4 44.2 43.1 44.5 40.5 46.8 y at 600 nm TA OD ₆₀₀ 1.8 4.4 16.3 32.4	Dry cell wt. (g/L) NT 10.01 NT 27.85 NT 28.00 30.99 32.29 BLE 8A Dry cell wt. (g/L) NT NT NT 20.33	(% w/v) 2.02 0.30 0.30 1.25 2.01 0.32 0.15 0.04 Xylose (% w/v) 4.35 3.81 2.83 4.53
Time (h) 0 24 30 48 54 78 102 120 D ₆₀₀ —Optical densit T—Not tested Time (h) 0 24 30 48	TAI OD ₆₀₀ 0.2 11.0 21.0 37.8 47.9 64.3 61.3 61.6 y at 600 nm TAI OD ₆₀₀ 0.1 12.0 22.2 42.9	Dry cell wt. (g/L) NT 6.52 NT 21.88 NT 34.06 37.65 40.64 BLE 6B Dry cell wt. (g/L) NT 6.92 NT 25.79	(% w/v) 2.09 0.61 0.38 1.29 1.62 2.66 1.24 0.74 Xylose (% w/v) 2.13 0.61 0.98 3.81	40 — 40 — 45 — 50 — OI NO	Time (h) 0 24 30 48 54 79 102 120 0e00—Optical densite—Not tested Time (h) 0 6 12	OD ₆₀₀ 0.1 15.4 22.4 44.2 43.1 44.5 40.5 46.8 y at 600 nm TA OD ₆₀₀ 1.8 4.4 16.3	Dry cell wt. (g/L) NT 10.01 NT 27.85 NT 28.00 30.99 32.29 BLE 8A Dry cell wt. (g/L) NT NT NT	(% w/v) 2.02 0.30 0.30 1.25 2.01 0.32 0.15 0.04 Xylose (% w/v) 4.35 3.81 2.83

OD₆₀₀—Optical density at 600 nm NT—Not tested

65 OD₆₀₀—Optical density at 600 nm NT—Not tested

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TABLE 8B

20 TABLE 10B-continued

Xylose (% w/v)	Dry cell wt. (g/L)	OD_{600}	Time (h)
3.24	NT	1.8	0
2.76	NT	5.2	6
1.72	NT	16.4	12
4.29	19.63	31.5	24
3.56	NT	35.2	30
1.82	30.07	46.5	48
1.43	32.55	51.1	54

 OD_{600} —Optical density at 600 nm

NT-Not tested

TABLE 9A

Time (h)	OD_{600}	Dry cell wt. (g/L)	Xylose (% w/v)
0	1.8	NT	3.78
6	4.5	NT	3.26
23	30.5	18.38	0.62
25	NT	NT	3.77
30	37.6	NT	3.14
47	46.8	27.97	1.19
54	46.6	NT	0.78

OD₆₀₀—Optical density at 600 nm NT—Not tested

TABLE 9B

ime (h)	OD ₆₀₀	Dry cell wt. (g/L)	Xylose (% w/v)	
0	1.8	NT	3.79	
6	5.0	NT	3.25	
23	27.7	16.99	0.74	
25	NT	NT	1.12	
30	31.7	NT	2.59	
47	46.5	26.31	1.46	
54	45.2	NT	1.04	

 OD_{600} —Optical density at 600 nm

NT-Not tested

TABLE 10A

	Xylose (percent, by weight)		Ethanol (percent, by volume)	
Time (h)	With Aeration	No Aeration	With Aeration	No Aeration
0	2.94	3.03	0.00	0.00
28	1.98	1.14	0.00	1.03
31	1.76	0.32	0.00	1.52
48	1.43	0.02	0.00	1.70
53	1.37	0.01	0.00	1.69

TABLE 10B

	Optical Density at 600 nm				
	No Aeration	With Aeration	Time (h)		
60	0.10	0.13	0		
	0.28	0.32	2		
	0.11	0.20	4		
	0.17	0.26	6		
	0.19	0.18	8		
	0.39	0.41	12		
65	2.47	5.51	23		
	3.29	7.78	26		

	Optical Densi	Optical Density at 600 nm		
Time (h)	With Aeration	No Aeration		
31	8.93	4.27		
48	9.90	4.45		

TABLE 11A

	Component	Concentration
_	Yeast Extract	5 g/L
	Urea	20 g/L
	Diammonium Phosphate	5.0 g/L
	Magnesium Sulfate Heptahydrate	0.8 g/L
	Zinc Sulfate Heptahydrate	0.03 g/L
	Lactoside 247	5 PPM

*In Water

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TABLE 11B

Time (h)	OD ₆₀₀	Dry cell wt. (g/L)	Xylose (percent)
0	1.8	NT	3.79
6	5.0	NT	3.25
23	27.7	16.99	0.74
25	NT	NT	1.12
30	31.7	NT	2.59
47	46.5	26.31	1.46
54	45.2	NT	1.04

OD₆₀₀—Optical density at 600 nm

NT-Not tested 35

TABLE 11C

Time (l	h) OD ₆₀₀	Dry cell wt (g/L)	. Xylose (percent)
0	1.7	NT	3.69
6	5.1	NT	3.20
23	31.8	19.07	0.29
25	NT	NT	0.79
30	38.1	NT	1.92
47	46	27.41	0.62
52	49.1	NT	0.43

 OD_{600} —Optical density at 600 nm

NT-Not tested

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We claim:

1. A method of propagating ethanologen for use in the production of a fermentation product from biomass comprising the steps of:

providing a medium for propagation of ethanologen; supplying a first cell mass of ethanologen to the medium; supplying xylose to the medium as a carbon source for cell

mass growth of the ethanologen;

maintaining the medium comprising the first cell mass of ethanologen at a pH of between about 5.0 and 6.0 and at a temperature of between about 26 and about 37 degrees Celsius so that the first cell mass of ethanologen is propagated into a second cell mass of ethanologen;

aerating the medium so that the first cell mass of ethanologen is propagated into a second cell mass of ethanolo-

and wherein, the second cell mass of ethanologen is at least 200 times larger than the first cell mass of ethanologen.

- 2. The method of claim 1 wherein xylose is the sole source of carbon supplied to the medium.
- 3. The method of claim 2 wherein the ethanologen is derived from Saccharomyces cerevisiae.
- 4. The method of claim 2 wherein xylose is supplied to the 5 medium at a concentration of at least 1 percent by weight of
- 5. The method of claim 2 wherein the step of providing a first medium for propagation of the ethanologen comprises a first stage and further comprising the steps of:
 - providing a second medium for propagation of ethanologen in a second stage;
 - supplying the second cell mass of ethanologen to the second medium;
 - maintaining the second medium comprising the second 15 cell mass of ethanologen at a pH of between about 5.0 and 6.0 and at a temperature of between about 26 and about 37 degrees Celsius so that the second cell mass of ethanologen is propagated into a third cell mass of etha-
 - wherein the third cell mass of ethanologen has a cell mass that is larger than the cell mass of the second cell mass of ethanologen.
- 6. The method of claim 5 wherein xylose is provided to the second medium as a carbon source for the ethanologen in the 25 second stage.
- 7. The method of claim 1 wherein the biomass comprises lignocellulosic material.
- 8. The method of claim 7 wherein the xylose supplied to the medium is obtained from the lignocellulosic material.
- 9. The method of claim 8 wherein xylose is obtained as a component of the biomass and wherein xylose is supplied to the medium comprises at a rate of at least 0.12 grams of xylose per minute.
- 10. The method of claim 9 wherein the component com- 35 prises xylose and glucose and the ethanologen comprises an organism capable of fermenting xylose into ethanol and glucose into ethanol.
- 11. The method of claim 1 wherein aerating the medium comprises the step of supplying the medium with an airflow 40 production of a fermentation product from biomass in a ferof at least 1.0 volumes of air per volume of medium per
- 12. The method of claim 1 wherein aerating the medium comprises maintaining the medium under aerobic conditions by supplying airflow of at least 1.0 liters per liter of medium 45 per minute so that xylose is used for cell growth instead of production of ethanol.
- 13. The method of claim 1 wherein the ethanologen comprises yeast cells capable of fermenting xylose into ethanol.
- 14. The method of claim 1 further comprising the step of 50 providing an agent to the medium; wherein the agent comprises at least one nutrient.
- 15. The method of claim 14 wherein the agent comprises at least one of yeast extract, urea, diammonium phosphate, magnesium sulfate or zinc sulfate.
- 16. The method of claim 1 wherein the xylose is supplied to the medium in an amount so that the initial concentration of xylose is at least 20 grams of xylose per liter of medium.
- 17. A method of propagating ethanologen for use in the production of a fermentation product from biomass compris- 60 ing the steps of:
 - providing a medium for propagation of ethanologen; supplying a first cell mass of ethanologen to the medium; providing an agent to the medium;
 - providing a component obtained from the biomass to the 65 medium, wherein the component comprises xylose as a carbon source for the ethanologen;

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- maintaining the medium comprising the first cell mass of ethanologen at a pH of between about 5.0 and 6.0 and at a temperature of between about 26 and about 37 degrees Celsius so that the first cell mass of ethanologen is propagated into a second cell mass of ethanologen;
- aerating the medium so that the first cell mass of ethanologen is propagated into a second cell mass of ethanolo-
- wherein the second cell mass of ethanologen is at least 200 times larger than the first cell mass of ethanologen;
- wherein the biomass comprises lignocellulosic material;
- wherein the lignocellulosic material comprises at least one of corn cobs, corn plant husks, corn plant leaves and corn plant stalks;
- wherein the component is obtained from the lignocellulosic material;

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- wherein the ethanologen comprises yeast cells capable of fermenting xylose into ethanol.
- 18. The method of claim 17 wherein the step of supplying the component to the medium comprises xylose supplied at a rate of at least 0.12 grams of xylose per minute.
 - 19. The method of claim 17 further comprising the steps of: providing a second medium for propagation of ethanolo-
 - supplying the second cell mass of ethanologen to the second medium:
 - maintaining the second medium comprising the second cell mass of ethanologen at a pH of between about 5.0 and 6.0 and at a temperature of between about 26 and about 37 degrees Celsius so that the second cell mass of ethanologen is propagated into a third cell mass of ethanologen:
 - wherein the third cell mass of ethanologen has a cell mass that is larger than the cell mass of the second cell mass of ethanologen.
- 20. A system for propagating ethanologen for use in the mentation system comprising:
 - a first stage comprising a first vessel configured to contain a medium comprising ethanologen;
 - a second stage comprising a second vessel configured to contain a medium supplied from the first stage;
 - a source of xylose to be provided to the medium as a carbon source for ethanologen in the first stage;
 - a source of xylose to be provided to the medium as a carbon source for the ethanologen in the second stage;
 - wherein the ethanologen has a first cell mass when supplied to the first stage and the ethanologen has a second cell mass at least 200 times larger than the first cell mass when supplied from the first stage to the second stage and the ethanologen has a third cell mass at least 20 times larger than the second cell mass when supplied from the second stage;
 - wherein the first vessel is configured to aerate the medium and maintain the medium at a pH of between about 5.0 and 6.0 and at a temperature of between about 26 and about 37 degrees Celsius so that ethanologen can be propagated into the second cell mass; and
 - wherein the second vessel is configured to aerate the medium and maintain the medium at a pH of between about 5.0 and 6.0 and at a temperature of between about 26 and about 37 degrees Celsius so that ethanologen can be propagated into the third cell mass.

21. The system of claim 20 further comprising an apparatus to pre-treat the biomass into a liquid component comprising the source of xylose for the ethanologen.

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